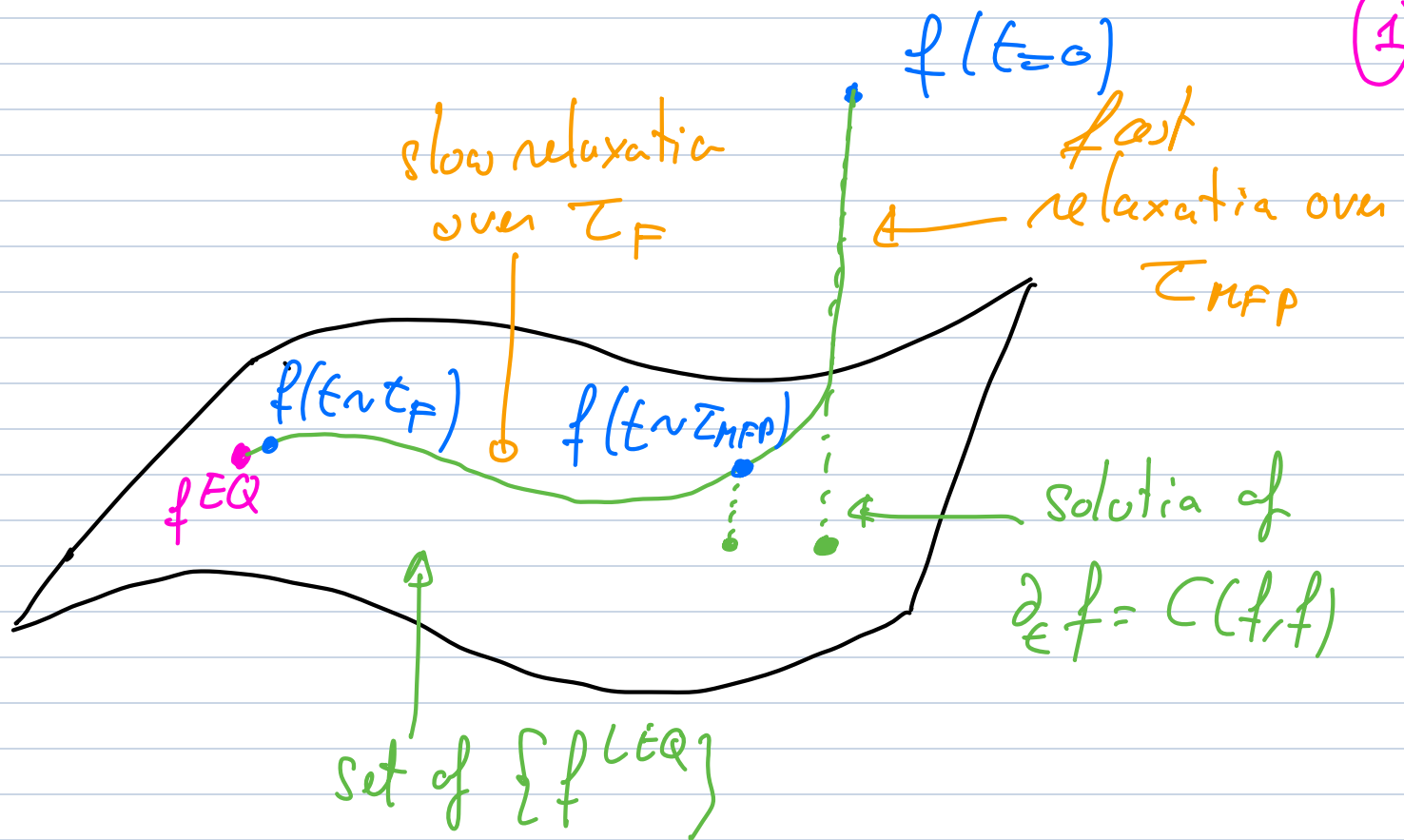


(1)



$$\underline{BE}: \partial_\epsilon f + \underbrace{\frac{\partial f}{\partial \vec{q}} \cdot \frac{\vec{p}}{m}}_{\equiv \frac{1}{\tau_F} L_F f} = \underbrace{C(f, f)}_{\equiv \frac{1}{\tau_{HFP}} \hat{C}(f, f)}; t = \hat{t} \tau_F; \epsilon = \frac{\tau_{HFP}}{\tau_F}$$

$$f(\vec{q}, \vec{p}, t) = f_0(\vec{q}, \vec{p}, t) + \epsilon f_1(\vec{q}, \vec{p}, t) + O(\epsilon^2)$$

Order by order:

$$O(\frac{1}{\epsilon}) \quad 0 = C(f_0, f_0) \Rightarrow f_0 = f^{LEQ}$$

$$O(1) \quad \partial_{\hat{t}} f_0 + L_1 f_0 = \hat{C}(f_0, f_1) + \hat{C}(f_1, f_0) \simeq -f_1$$

Leading order

$$f_0(\vec{q}, \vec{p}, t) = f^{LEQ}(\vec{p}, \vec{q}) = \tilde{\gamma}(q, t) e^{-\vec{\omega}(\vec{q}, t) \cdot \vec{p} - \beta(\vec{q}, t) \left[\frac{\vec{p}^2}{2m} + v(\vec{q}) \right]}$$

Characterized by

(2)

density field $n(\vec{q}, t) = \int d\vec{p} f(\vec{q}, \vec{p}, t)$

velocity field $\vec{u}(\vec{q}, t) = \frac{1}{n} \int d\vec{p} f(\vec{q}, \vec{p}, t) \vec{v} \equiv \langle \vec{v}^2 \rangle_{f(\vec{q}, \vec{p}, t)}$

energy
temperature fields $\left\{ \begin{array}{l} \varepsilon = \langle \frac{1}{2} m \delta \vec{v}^2 \rangle = \frac{1}{2} m (\langle \vec{v}^2 \rangle - \vec{u}^2) \\ T(\vec{q}, t) = \frac{2}{3} \frac{\varepsilon(\vec{q}, t)}{k_B} \text{ such that } \varepsilon = \frac{3}{2} k_B T \end{array} \right.$

Evolution of the slow fields

$$D_t n \equiv (\partial_t + u_\alpha \partial_{q_\alpha}) n = -n \partial_{q_\alpha} u_\alpha$$

$$M D_t u_\alpha = -\frac{1}{n} \partial_{q_\beta} \cdot P_{\alpha\beta} \Leftrightarrow M D_t \vec{u} = -\frac{1}{n} \vec{\nabla} \cdot \vec{P}$$

with $P_{\alpha\beta} = M n \langle (u_\alpha - v_\alpha)(u_\beta - v_\beta) \rangle = M n \langle \delta v_\alpha \delta v_\beta \rangle$

$$\partial_t T + u_\alpha \partial_\alpha T = -\frac{2}{3 n k_B} \partial_\alpha h_\alpha - \frac{2}{3 n k_B} P_{\alpha\beta} u_{\alpha\beta}$$

where

- $u_{\alpha\beta} = \frac{1}{2} (\partial_{q_\alpha} u_\beta + \partial_{q_\beta} u_\alpha)$ is called the strain rate tensor

- $h_\alpha = \frac{n M}{2} \langle \delta v_\alpha \delta v_\beta \delta v_\beta \rangle$ is the kinetic energy flux
along $\vec{u}_\alpha$, a.k.a. heat flux

Closure: To compute the evolution of $n, T, \vec{u}$, we need to

compute $P_{\alpha\beta} = m M \langle \delta v_\alpha \delta v_\beta \rangle$ & $h_\alpha = \frac{m M}{2} \langle \delta v_\alpha \delta v_\beta \delta v_\beta \rangle$,

which we can do perturbatively using f_0

$$f_0 \Rightarrow P_{\alpha\beta}^0, h_\alpha^0 \Rightarrow \partial_\epsilon (n, T, \vec{u})^0 \Rightarrow f_1 \Rightarrow P_{\alpha\beta}^1, h_\alpha^1 \Rightarrow \partial_\epsilon (n, T, \vec{u})^1 \text{ etc.}$$

Notation: A_0 or A^0 refers to the order of the approximation

2.4.3) Leading order dynamics

Given $n, T, \vec{u}$, we can determine f_0 through:

$$\left. \begin{aligned} \int f_0 d\vec{p} &= n(q) \\ \int \vec{v} f_0 d\vec{p} &= n(\vec{q}) \vec{u}(\vec{q}) \\ \int \frac{M}{2} (\vec{v} - \vec{u})^2 f_0 d\vec{p} &= n(\vec{q}) \varepsilon(\vec{q}) = \frac{3}{2} h_0 T(\vec{q}) \end{aligned} \right\} f_0(\vec{q}|\vec{p}, t) = \frac{n(\vec{q})}{[9\pi M h_0 T]^{3/2}} e^{-\frac{(\vec{p} - M\vec{u})^2}{2 M h_0 T}} = \frac{n}{(9\pi M h_0 T)^{3/2}} e^{-\frac{M \delta \vec{v}^2}{2 h_0 T}}$$

Pressure & heat flux

$$P_{\alpha\beta}^0 = m M \langle (v_\alpha - u_\alpha) (v_\beta - u_\beta) \rangle_0 = m M \cdot \delta_{\alpha\beta} \cdot \frac{h_0 T}{M} = m h_0 T \delta_{\alpha\beta}$$

$\Rightarrow$ Isotropic pressure given by ideal gas law

$h_x^0 = 0$ because it involves an odd moment of δv

(4)

Leading order dynamics

$$\partial_\epsilon m + u_\alpha \partial_{q_\alpha} m = -m \partial_{q_\alpha} u_\alpha \quad (1)$$

$$M \partial_\epsilon u_\alpha + M u_\beta \partial_{q_\beta} u_\alpha = -\frac{1}{m} \partial_{q_\alpha} [m h T] \quad (2)$$

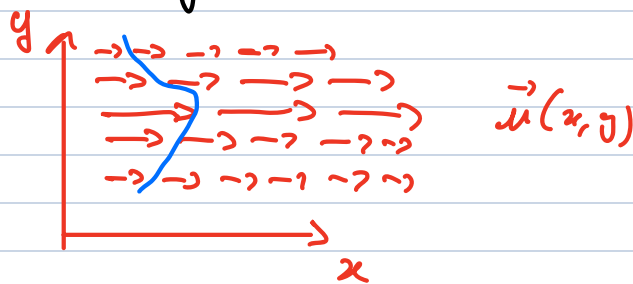
$$\partial_\epsilon T + u_\alpha \partial_{q_\alpha} T = -\frac{2}{3} T \partial_{q_\alpha} u_\alpha \quad (3)$$

At order 0, $f = f_0$ is left invariant by collisions but $\partial_\epsilon (u, u, T) \neq 0$
 $\Rightarrow$ induce some evolution of f_0 already $\Rightarrow$ maybe we are lucky & we get equilibration at leading order.

Does this dynamics relax?

let's consider an initial condition in which the gas is sheared

$$m = m_0 \text{ constant}, T = T_0 \text{ constant}, \vec{u} = u(y) \vec{e}_x$$



$$\left. \begin{aligned} \text{In eq (2), } \partial_{q_\alpha} (m_0 h T_0) &= 0 \\ u_\beta \partial_{q_\beta} \vec{u}_\alpha &= \delta_{\alpha x} \underbrace{u_y}_{=0} \partial_{q_y} \vec{u}_x = 0 \end{aligned} \right\} \partial_\epsilon \vec{u}_x = 0 \Rightarrow \vec{u} \text{ not relaxing to } \vec{u} = \vec{0} \dots$$

$\Rightarrow f^{\text{LEQ}}$ does not relax to f^{EQ} if we compute h & P to leading order 0-c

2.4.4) First order hydrodynamics

(5)

$$f_1 = -\tau_F \left[\partial_\epsilon f_0 + \frac{\vec{p}}{m} \cdot \partial_{\vec{q}} f_0 \right] \quad \text{easier than working with } \hat{\epsilon}.$$

$$f = f_0 + \frac{\tau_{\text{HFP}}}{\tau_F} f_1 = f_0 (1 + g_1)$$

$$-g_1 = \tau_{\text{HFP}} \left[\partial_\epsilon \ln f_0 + \frac{\vec{p}}{m} \cdot \partial_{\vec{q}} \ln f_0 \right] = \tau_{\text{HFP}} (\partial_\epsilon + v_\alpha \partial_{q_\alpha}) \left[\ln m - \frac{3}{2} \ln T - \frac{(\vec{v} - \vec{u})^2}{2k_B T} \right]$$

We need to compute g_1 to leading order in ϵ

$\Rightarrow$ use 0th order hydrodynamics for the right-hand-side

(i) use $\partial_\epsilon + v_\alpha \partial_{q_\alpha} = D_\epsilon + (v_\alpha - u_\alpha) \partial_{q_\alpha} = D_\epsilon + \delta v_\alpha \partial_{q_\alpha}$

(ii) leading order hydrodynamic equations

$$\begin{cases} D_\epsilon m = -m \partial_{q_\alpha} u_\alpha \\ m D_\epsilon u_\alpha = -\frac{1}{m} \partial_{q_\alpha} [m k_B T] \\ D_\epsilon T = -\frac{2}{3} T \partial_{q_\alpha} u_\alpha \end{cases}$$

$$\Rightarrow g_1 = -\frac{\tau_{\text{HFP}} m}{k_B T} u_{\alpha\beta} \left(\delta v_\alpha \delta v_\beta - \frac{\delta v^2}{3} \delta_{\alpha\beta} \right) - \frac{\tau_{\text{HFP}}}{T} \delta v_\alpha (\partial_{q_\alpha} T) \left(\frac{m}{2k_B T} \delta v^2 - \frac{5}{2} \right)$$

Proof:

$$\delta_{\alpha\beta} \partial_{q_\alpha} u_\beta = \delta_{\alpha\beta} u_{\alpha\beta}$$

$$\begin{aligned} -\frac{g_1}{\tau_{\text{HFP}}} &= -\partial_{q_\alpha} u_\alpha - \frac{3}{2} \left(-\frac{2}{3} \partial_{q_\alpha} u_\alpha \right) - \frac{m}{k_B T} \delta v_\alpha \frac{1}{m} \partial_{q_\alpha} [m k_B T] - \frac{m}{2k_B T} \delta v^2 \left(+\frac{2}{3T} \partial_{q_\alpha} u_\alpha \right) \\ &\quad + \delta v_\alpha \frac{\partial_{q_\alpha} m}{m} - \frac{3}{2T} \delta v_\alpha \partial_{q_\alpha} T + \frac{m}{k_B T} \delta v_\beta \delta v_\alpha \partial_{q_\alpha} u_\beta - \frac{1}{2} \frac{m}{k_B T} \delta v^2 \left(-\frac{1}{T^2} \delta v_\alpha \partial_{q_\alpha} T \right) \end{aligned}$$

$\delta v_\beta \delta v_\alpha u_{\alpha\beta}$

$$-\frac{g_1}{\tau_{HFP}} = -\delta v_\alpha \left[\frac{\partial q_\alpha^M}{n} + \frac{\partial q_\alpha^T}{T} - \frac{\partial q_\alpha^M}{n} + \frac{3}{2T} \partial q_\alpha^T \right] + \frac{M}{4T} \delta v_\alpha \delta v_\beta \mu_{\alpha\beta} - \frac{M}{34T} \delta \vec{r}^2 \delta_{\alpha\beta} \mu_{\alpha\beta} \quad (6)$$

$$+ \frac{M}{24T} \delta \vec{r}^2 \delta v_\alpha \frac{\partial q_\alpha^T}{T}$$

$$-\frac{g_1}{\tau_{HFP}} = \frac{M}{4T} \mu_{\alpha\beta} \left(\delta v_\alpha \delta v_\beta - \frac{\delta \vec{r}^2}{3} \delta_{\alpha\beta} \right) + \frac{\delta v_\alpha \partial q_\alpha^T}{T} \left(\frac{M}{24T} \delta \vec{r}^2 - \frac{5}{2} \right)$$

(ii) Compute μ & P to $O(\epsilon)$

$$f = f_0(1+g_1) \Rightarrow \langle O \rangle_f = \langle O(1+g_1) \rangle_{f_0}$$

$$P_{\alpha\beta} = m M \langle \delta v_\alpha \delta v_\beta \rangle = m M \langle \delta v_\alpha \delta v_\beta \rangle_0 - \frac{m \tau_{HFP} M^2}{4T} \mu_{\gamma\delta} \left[\langle \delta v_\alpha \delta v_\beta \delta v_\gamma \delta v_\delta \rangle_0 - \frac{1}{3} \delta_{\gamma\delta} \langle \delta v_\alpha \delta v_\beta \delta \vec{r}^2 \rangle_0 \right] + O(\epsilon)$$

$\underbrace{\langle \delta v \dots \delta v \rangle}_{\text{odd \# of terms}}$

Wick theorem:

$$\langle \delta v_\alpha \delta v_\beta \delta v_\gamma \delta v_\delta \rangle_0 = (\delta_{\alpha\beta} \delta_{\gamma\delta} + \delta_{\alpha\gamma} \delta_{\beta\delta} + \delta_{\alpha\delta} \delta_{\beta\gamma}) \underbrace{\langle \delta v_\alpha^2 \rangle \langle \delta v_\beta^2 \rangle}_{\frac{(k_B T)^2}{M^2}}$$

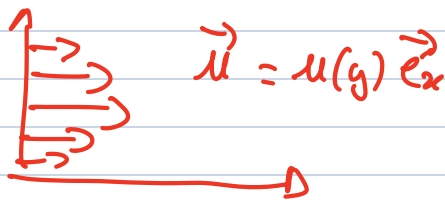
$$\mu_{\gamma\delta} \langle \delta v_\alpha \delta v_\beta \delta v_\gamma \delta v_\delta \rangle_0 = \frac{(k_B T)^2}{M^2} [2 \mu_{\alpha\beta} + \mu_{\gamma\gamma} \delta_{\alpha\beta}]$$

$$\langle \delta v_\alpha \delta v_\beta \delta v_\gamma \delta v_\gamma \rangle_0 = \frac{(k_B T)^2}{M^2} \left[\underbrace{\delta_{\alpha\beta} \delta_{\gamma\gamma}}_3 + 2 \underbrace{\delta_{\alpha\gamma} \delta_{\beta\gamma}}_{\delta_{\alpha\beta}} \right] = 5 \delta_{\alpha\beta} \frac{(k_B T)^2}{M^2}$$

$$\Rightarrow P_{\alpha\beta}^{(1)} = m k_B T \delta_{\alpha\beta} - m k_B T \tau_{HFP} \left[2 \mu_{\alpha\beta} + \mu_{\gamma\gamma} \delta_{\alpha\beta} - \frac{5}{3} \delta_{\alpha\beta} \mu_{\gamma\gamma} \right]$$

$$P_{\alpha\beta}^{(1)} = m k_B T \delta_{\alpha\beta} - 2 m k_B T \tau_{HFP} \mu_{\alpha\beta} + \frac{2}{3} m k_B T \delta_{\alpha\beta} \tau_{HFP} \partial_\gamma \mu_\gamma$$

Relaxation of shear flows:



(7)

$$\mu_{\alpha\beta} = \frac{1}{2} [\partial_\alpha \mu_\beta + \partial_\beta \mu_\alpha] = \frac{1}{2} [\delta_{\alpha y} \delta_{\beta x} + \delta_{\beta y} \delta_{\alpha x}] \mu'(y)$$

$$P_{\alpha\beta} = m h_B T \delta_{\alpha\beta} - m \tau_{HFP} h T [\delta_{\alpha y} \delta_{\beta x} + \delta_{\alpha x} \delta_{\beta y}] \mu'(y) \Rightarrow \text{not diagonal}$$

$$M \partial_\epsilon \mu_\alpha = - \frac{1}{m} \partial_{q_\beta} P_{\alpha\beta}$$

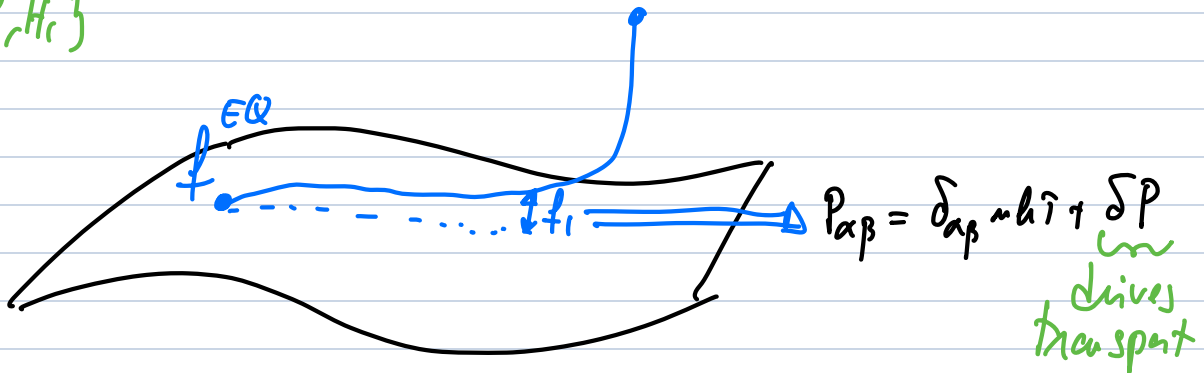
$$M \partial_\epsilon \mu_x + M \mu_x \cdot \underbrace{\partial_x \mu_x}_{=0} + M \mu_y \cdot \underbrace{\partial_y \mu_x}_{=0} = - \frac{1}{m} \partial_y (-m \tau_{HFP} h T \mu'(y))$$

$$\Rightarrow \partial_\epsilon \mu_x = \underbrace{\frac{\tau_{HFP} h T}{m}}_{\eta} \partial_{yy} \mu(y) \quad \swarrow m = m_0$$

η is the kinematic viscosity ($\mu = m M \eta$ is the dynamic viscosity).

What drives the relaxation to $\vec{u} \rightarrow 0$ & equilibrium?

- ① f_i alters the statistics of f and the values of $P_{\alpha\beta}, h_\alpha$
- ② transport then makes the conserved field relax $\{f, h_i\}$



Comment: one can also compute the heat flux $h_\alpha = -k \partial_{q_\alpha} T$

$$k \text{ is the thermal conductivity, } k = \frac{5}{2} \frac{m}{M} \tau_c h_B^2 T$$

Proof:

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$$* h_\alpha = \frac{mM}{2} \langle \delta v_\alpha \delta \vec{v}^2 (1+g_1) \rangle_0 \rightarrow \text{only even powers matter}$$

$\rightarrow \text{odd} \rightarrow \text{in } g_1$

$$h_\alpha = -\frac{mM T_{\text{eff}}}{2T} \left(\partial_{q_\beta} \right) \left\langle \frac{M}{2hT} (\delta \vec{v}^2)^2 \delta v_\beta \delta v_\alpha - \frac{5}{2} \delta \vec{v}^2 \delta v_\alpha \delta v_\beta \right\rangle$$

$$* \text{We need to compute } \langle \delta v_\delta \delta v_\gamma \delta v_\varepsilon \delta v_\zeta \delta v_\alpha \delta v_\beta \rangle = \frac{L^3 T^3}{M^3} \delta_{\alpha\beta} \times (\text{combinatorial factor})$$

All possible pairings (1) Graph strategy

$$\left. \begin{array}{l} \delta \bigcirc \delta \rightarrow \delta_{\delta\delta} = 3 \\ \delta \text{---} \delta \rightarrow \delta_{\alpha\beta} \\ \varepsilon \bigcirc \varepsilon \rightarrow \delta_{\varepsilon\varepsilon} = 3 \end{array} \right\} 9 \delta_{\alpha\beta}$$

$$\left. \begin{array}{l} \alpha \text{---} \beta \rightarrow \delta_{\alpha\beta} \\ \begin{array}{c} \varepsilon \quad \delta \\ \diagup \quad \diagdown \\ \delta \quad \varepsilon \end{array} \rightarrow x 2 \delta_{\varepsilon\varepsilon} = 6 \end{array} \right\} 6 \delta_{\alpha\beta}$$

$$\left. \begin{array}{l} \alpha \text{---} \varepsilon \text{---} \varepsilon \text{---} \beta \\ \delta \bigcirc \delta \rightarrow x 3 \end{array} \right\} 6 \delta_{\alpha\beta}$$

$$\alpha \text{---} \varepsilon \text{---} \varepsilon \text{---} \delta \text{---} \delta \text{---} \beta \rightarrow 4 \delta_{\alpha\beta}$$

$x 2 \quad x 2$

$$\left. \begin{array}{l} \alpha \text{---} \delta \text{---} \delta \text{---} \beta \\ \varepsilon \bigcirc \varepsilon \rightarrow 3 \end{array} \right\} 6 \delta_{\alpha\beta}$$

$$\alpha \text{---} \delta \text{---} \delta \text{---} \varepsilon \text{---} \varepsilon \text{---} \beta \rightarrow 4 \delta_{\alpha\beta}$$

$$\Rightarrow 35 \delta_{\alpha\beta}$$

(2) Math strategy. Sum only if $\sum$ explicit.

$$\sum_{\varepsilon, \delta} \langle \delta v_\alpha \delta v_\beta \delta v_\varepsilon \delta v_\zeta \delta v_\gamma \delta v_\gamma \rangle = \delta_{\alpha\beta} \langle \delta v_\alpha^2 \sum_{\varepsilon} \delta v_\varepsilon^2 \sum_{\delta} \delta v_\delta^2 \rangle$$

$$= \delta_{\alpha\beta} \left[\langle \delta v_\alpha^6 \rangle_{\varepsilon=\delta=\alpha} + 2 \sum_{\varepsilon \neq \alpha} \langle \delta v_\alpha^4 \delta v_\varepsilon^2 \rangle_{\delta=\alpha} \right.$$

$$\left. + \sum_{\varepsilon \neq \alpha} \langle \delta v_\alpha^2 \delta v_\varepsilon^4 \rangle + \sum_{\varepsilon \neq \delta \neq \alpha} \langle \delta v_\alpha^2 \delta v_\varepsilon^2 \delta v_\delta^2 \rangle \right]$$

$$= \delta_{\alpha\beta} \left[5 \langle \delta v_{\alpha}^2 \rangle \langle \delta v_{\alpha}^4 \rangle + 4 \langle \delta v_{\alpha}^4 \rangle \langle \delta v_{\epsilon}^2 \rangle \right.$$

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$$+ 2 \langle \delta v_{\alpha}^2 \rangle \langle \delta v_{\epsilon}^4 \rangle + 2 \langle \delta v_{\alpha}^2 \rangle \langle \delta v_{\epsilon}^2 \rangle \langle \delta v_{\gamma}^2 \rangle \Big]$$

$$= \delta_{\alpha\beta} \left[15 \left(\frac{\hbar \beta T}{m} \right)^3 + 12 \left(\frac{\hbar \beta T}{m} \right)^3 + 6 \left(\frac{\hbar \beta T}{m} \right)^3 + 2 \left(\frac{\hbar \beta T}{m} \right)^3 \right]$$

$$= 35 \left(\frac{\hbar \beta T}{m} \right)^3 \delta_{\alpha\beta}$$

$$h_{\alpha} = - \frac{m H \tau_{HFP}}{2T} \left(\partial_{q_{\beta}} T \right) \left\langle \frac{m}{2\hbar T} (\delta \vec{v}^2)^2 \delta v_{\beta} \delta v_{\alpha} - \frac{5}{2} \delta \vec{v}^2 \delta v_{\alpha} \delta v_{\beta} \right\rangle$$

$$= - \frac{m H \tau_{HFP}}{4T} \left(\partial_{q_{\beta}} T \right) \delta_{\alpha\beta} \left(\frac{m}{4T} \cdot 35 \left(\frac{\hbar \beta T}{m} \right)^3 - 25 \left(\frac{\hbar \beta T}{m} \right)^2 \right)$$

$$h_{\alpha} = - \frac{5}{2} \frac{m}{m} \tau_{HFP} \hbar^2 T \left(\partial_{q_{\alpha}} T \right)$$

First-order hydrodynamics

$$D_{\epsilon} n = -n \partial_{q_{\alpha}} u_{\alpha}$$

$$M D_{\epsilon} u_{\alpha} = - \frac{1}{m} \partial_{q_{\beta}} \cdot P_{\alpha\beta} = - \frac{1}{m} \partial_{q_{\alpha}} \left(m \hbar \beta T + \frac{2}{3} m \hbar \beta T \tau_{HFP} \partial_{\gamma} u_{\gamma} \right) \\ + \frac{1}{m} \partial_{q_{\beta}} \left[m \hbar \beta T \tau_{HFP} u_{\alpha\beta} \right]$$

$$D_{\epsilon} T = \frac{5}{3m \hbar \beta} \partial_{q_{\alpha}} \left[\frac{m}{m} \tau_{HFP} \hbar^2 T \partial_{q_{\alpha}} T \right] - \frac{2T}{3} \left[\partial_{\alpha} u_{\alpha} - \tau_{HFP} u_{\alpha\beta} u_{\alpha\beta} + \frac{2}{3} \tau_{HFP} (\partial_{\alpha} u_{\alpha})^2 \right]$$

Relaxation to equilibrium

$$n = n_0 + \delta n; \quad u = \delta u; \quad T = T_0 + \delta T$$

$$\Rightarrow \text{linearized dynamics for } \begin{pmatrix} \delta n \\ \delta u \\ \delta T \end{pmatrix} : \quad \partial_{\epsilon} \begin{pmatrix} \delta n \\ \delta u \\ \delta T \end{pmatrix} = M \cdot \begin{pmatrix} \delta n \\ \delta u \\ \delta T \end{pmatrix}$$

The eigenvalues of M have negative real parts, leading to the decay of the perturbation and the convergence to n & T uniform and $\vec{u} = \vec{0} \Rightarrow$ global equilibrium.